

# HIGH FREQUENCY ELECTRONIC BALLASTS

ELECTRONIC  
FLUORESCENT



**ADVANCE**

ADVANCE, 10275 WEST HIGGINS ROAD, ROSEMONT, IL 60018. TEL: (847) 390-5000, FAX: (847) 390-5109

## Electronic Ballast Fundamentals

### The job of a ballast

In all fluorescent lighting systems, the ballast's basic tasks include:

- Providing the proper voltage to establish an arc between the two electrodes.
- Regulating the electric current flowing through the lamp to stabilize light output.

In some fluorescent lighting systems, the ballast also provides a controlled amount of electrical energy to preheat or maintain the temperature of the lamp electrodes at levels specified by the manufacturer. This is required to prevent electrode filaments deteriorating prematurely and shortening the lamp life.

### Starting Methods

For many years there were only three types of lighting systems: preheat, rapid start and slimline instant start. With the introduction of electronic ballasts, two additional types of lighting system circuits have been added: instant start for T8 lamps and programmed start. Each requires a special ballast design to operate the lamps in the circuit properly.

**Instant start electronic ballasts** start lamps without delay (<0.1 seconds) or flicker by providing a starting voltage that is sufficiently high to start a discharge through the lamps without the need for heating lamp electrodes. For F32T8 systems, the starting voltage is about 600V. The elimination of electrode heating maximizes energy savings – typically saving two watts per lamp compared to rapid start ballasts. Instant start ballasts are best suited for applications with limited switches each day. Lamps operated by instant start ballasts typically operate 10,000 to 15,000 switch cycles before failure.

**Rapid start electronic ballasts** start lamps quickly (0.5 – 1.0 seconds) without flicker by heating the lamp electrodes and simultaneously applying a starting voltage. The starting voltage of about 500V for F32T8 systems is sufficient to start a discharge through the lamps when the electrodes have reached an adequate temperature. Electrode heating continues during operation and typically consumes two watts per lamp. Lamps operated by rapid start ballasts typically operate 15,000 to 20,000 switch cycles before failure.

**Programmed start electronic ballasts** also start lamps quickly (1.0 -1.5 seconds) without flicker. Programmed start ballasts are designed to provide maximum lamp life in frequent lamp starting applications such as in areas where occupancy sensor controls are used. Programmed start electronic ballasts precisely heat the lamp electrodes, tightly controlling the preheat duration before applying the starting voltage. This enhancement over rapid start ballasts minimizes electrode stress and depletion of emitter material, thereby maximizing lamp life. Lamps operated by programmed start ballasts typically operate up to 50,000 switch cycles before failure.

### Circuits

**Series vs. Parallel.** Lighting systems are typically wired in a series or parallel circuit. When a ballast is operating multiple lamps in a series circuit, if one lamp fails, the circuit is opened and all the lamps will extinguish. When a ballast operates multiple lamps in a parallel circuit, the lamps operate independently of each other so, if one lamp fails, the others can keep operating as the circuit between them and the ballast remains unbroken.

As a general rule, rapid start ballasts are wired with the lamps in series. Programmed start ballasts are also typically wired with lamps in series. However, some three- and four-lamp ballasts feature series-parallel operation; so that when a single lamp in one branch fails, the lamp(s) in the parallel branch will continue to operate. Instant start ballasts are typically wired with the lamps in parallel.

### The Language of Ballasts

**Input Voltage (dedicated vs. multi).** Most ballasts are designed to operate at specific voltages. Newer electronic ballasts, including Advance models that use IntelliVolt® technology, offer much greater flexibility and other advantages such as inventory reduction. Today's increasing demands on electrical utilities can cause wide voltage variations during load demand changes which in turn cause light output from lamps operated on dedicated electronic and electromagnetic ballasts to vary with the input voltage changes. With IntelliVolt technology, many Advance ballasts maintain constant light output through nominal input voltage ranges of 120 to 277 volts, thereby compensating for any change in input voltage. Some ballasts operate from 277 to 480 volts or 347 to 480 volts.

**Input Watts/ANSI Watts.** Input watts published by ballast manufacturers are the total watts consumed by both the ballast and the lamps it operates. ANSI watts are the rating given for a ballast measured under the strict testing procedures specified by ANSI standards and are the only dependable measure of this performance. Energy savings can be determined by comparing the input watts of different lighting systems.

Input watts may be affected by tolerance build-up from the ballast, lamp, input voltage and ambient temperature. The input watts published in this catalog are for nominal conditions only.

**Ballast Factor (BF)** is the ratio of light output from a lamp operated on a commercial ballast to the light output of that same lamp operated on a "reference ballast" as specified by ANSI standards. Light output ratings published by lamp manufacturers, are based on this "reference ballast".

$$BF = \frac{\text{light output of lamp operated on commercial ballast}}{\text{light output of lamp operated on reference ballast}}$$

BF is a measure of light output best thought of as a 'multiplier'. Multiplying the BF times rated lumens will determine actual light output of a given system operated on commercial ballasts.

**Ballast Efficacy Factor (BEF)** is the ratio of ballast factor to input watts. This measurement is generally used to compare the efficiency of various lighting systems – higher numbers being more efficient.

$$\text{Ballast Efficacy Factor} = \frac{\text{Ballast Factor} \times 100}{\text{Input Watts}}$$

This comparison is only valid, however, for ballasts operating the same number and type of lamps. In order to compare different types of lighting systems, the lumen output of the lamps must also be used. For more information, see "The ABC's of Electronic Fluorescent Ballasts".

**Power Factor (PF)** is the measurement of how effectively a ballast converts the voltage and current supplied by the power source into watts of usable power delivered to the ballast and lamps. Perfect power utilization would result in a power factor of one.

$$PF = \frac{\text{Input Watts}}{\text{Input Current} \times \text{Input Voltage}}$$

A ballast's power factor may be classified under any one of the following categories:

High Power Factor (HPF)	0.90 or greater
Power Factor Corrected (PFC)	0.80 to 0.89
Normal (Low) Power Factor (NPF)	0.79 or less

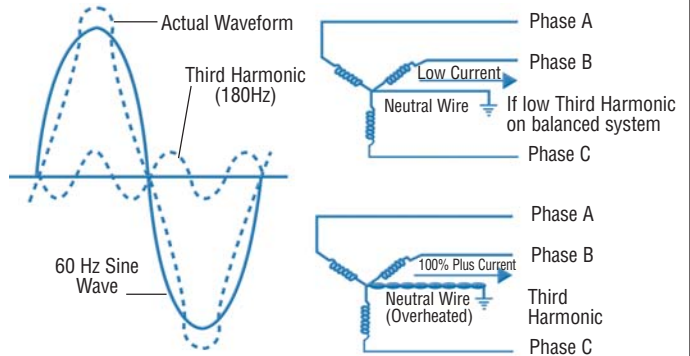
Power factor measurements pertain only to the effective use of power supplied to the ballast. They are not an indication of the ballast's ability to supply light through the lamps. Because low power factor ballasts require about twice the current needed by high power factor ballasts, they allow fewer fixtures per circuit and create added wiring costs. High power factor ballasts are generally specified for all commercial lighting applications.

**EMI/RFI.** Because they operate at high frequency, electronic ballasts may produce electromagnetic interference (EMI) or radio frequency interference (RFI). RFI frequencies are a subset of EMI frequencies. EMI issues cover all possible operating frequencies while RFI is only concerned with radio and television frequencies. This interference could affect the operation of sensitive electrical equipment, such as radios, televisions or medical equipment. All Advance electronic ballasts incorporate features necessary to afford maximum protection for the operating environment and operate well within regulatory limits. For more information, see "The ABC's of Electronic Fluorescent Ballasts".

**Ballast Noise.** The slight "humming" sound associated with fluorescent lighting systems results from vibration caused by the inherent electromagnetic action in the core-and-coil assembly of the ballasts. All electromagnetic and some electronic ballasts make this sound. Ballasts are assigned a sound rating, "A" through "F", based on the amount of sound produced, with "A" being the quietest. Generally, the larger the lamp and ballast, the higher the sound level and the sound rating will be. Because electronic ballasts have smaller components, they have the lowest sound rating. Some electronic ballasts make almost no sound. There is no ANSI standard for this rating and it is left up to the manufacturer to rate their ballasts.

**Inrush Current.** All electrical devices including ballasts have an initial current surge that is greater than their steady-state operating current. A new standard published by the National Electrical Manufacturers Association (NEMA) – NEMA 410 – Performance Testing for Lighting Controls and Switching Devices with Electronic Fluorescent Ballasts – covers worst-case ballast inrush currents. All circuit breakers and light switches are designed for inrush currents. The electrical system should be designed with this issue in mind.

**Total Harmonic Distortion (THD).** Harmonic distortion occurs when the wave-shape of current or voltage varies from a pure sine wave. Except for a simple resistor, all electronic devices, including electromagnetic and electronic ballasts, contribute to power-line distortion. For ballasts, THD is generally considered the percent of harmonic current the ballast adds to the power distribution system. The ANSI standard for electronic ballasts specifies a maximum THD of 32% for commercial applications. However, most electric utilities now require that the THD of electronic ballasts be 20% or less. Almost all Advance electronic ballasts are rated for either less than 20% THD or less than 10% THD.



Indicates ballast is listed with Underwriters Laboratories, Inc. and complies with UL935 Standard for Fluorescent Lamp Ballasts (File No. E14927).

Visit [www.ul.com](http://www.ul.com) to find a current listing of Advance ballasts under File No. E14927.



Indicates ballast is certified by Canadian Standards Association and complies with CSA C22.2 No. 74 Standard for Fluorescent Lamp Ballasts (File No. 007310)

Visit [www.csa.ca](http://www.csa.ca) to find current listing of Advance ballasts under File No. 007310.

Normal Input Voltage	Catalog Number Prefix Code	Label Color Coding
120V	R	Yellow
277V	V	Red
347V	G	Grey
120V to 277V	I	Blue
277V to 480V	J	Brown
347V to 480V	H	Purple

## Total Harmonic Current

### Non-Dimming Applications

When selecting a ballast for a lighting application, the Total Harmonic Current (THC) rating of the ballast is more significant than Total Harmonic Distortion (THD). This is because the absolute value of harmonic current, not the percentage, affects the electrical power distribution system. As can be seen in the table on page 1-12, the THC rating of our *Standard* 2-lamp electronic T8 lamp ballast is well below that of both the conventional and energy-

saving magnetic T12 lamp ballasts it replaces. Moreover, the THC rating of our *Centium* electronic ballast is even lower.

### Dimming Applications

#### Mark 7® 0-10V and ROVR

Traditional low voltage controlled ballasts and ROVR™ typically produce less than 10% THD at full light output and less than 20% THD throughout the entire dimming range, but require extra wires for the control circuit. THC is always lower than that of the conventional or energy-saving magnetic system.

#### Mark 10® Powerline

Mark 10® *Powerline* electronic dimming ballasts are controlled by 2-wire modified powerline phase-cut style line voltage dimmers. Whenever the ballast is dimmed, the input voltage is cut or “chopped”, causing the THD and THC to increase and the Power Factor to decrease.

Mark 10® *Powerline* electronic dimming systems (ballast and controller) have similar THD and Power Factor levels as the conventional lighting systems they replace. Since a much smaller load is required by the Mark 10® *Powerline* electronic dimming system to achieve the same illumination level as a magnetic ballast system (20-30% less), the total input current will be considerably less. As a result, the magnitude of the total harmonic current will be less.

For example, a typical Mark 10® *Powerline* electronic ballast and dimmer control might draw a line current of 0.58A at 15% THD at full light output. If the light level is reduced to 5% of the maximum, the input power is decreased to 0.19A at 95% THD. While the THD level may seem alarmingly high at the 5% max-

imum light output setting, the total harmonic current is still lower (0.13A) than the conventional T12 magnetic system (0.20A). Moreover, the overall heating effect on the wires and the distribution transformer is never higher than the existing conventional or energy saving T12 magnetic systems.<sup>1</sup>

### Conclusions

Our analysis demonstrates that a simple ballast retrofit to electronic ballasts *will not* cause harmonic problems if none existed before the retrofit. Also, in new fixture applications, total harmonic distortion should not be a concern when specifying electronic ballasts. Finally, it is important to remember that electronic ballasts are not the greatest source of THD in an electrical distribution system. Other electronic devices such as computers, laser printers, and other electronic equipment can draw current with more than 100% THD in some cases.

**Table 1: Comparison of THD and THC Levels**

Advance Part No.	Ballast Type	Light Output Setting	Lamp Type	Input Current	% THD	%THC <sup>2</sup>
RQM-2S40-TP	Conventional Magnetic	100% (Ballast Factor is 0.98)	(2) F40T12	0.84A	<25%	<b>0.20A</b>
R2S40-TP	Energy Saving Magnetic	100% (Ballast Factor is 0.95)	(2) F34T12	0.63A	<20%	<b>0.12A</b>
REL-2P32-SC	<i>Standard</i> Electronic	100% (Ballast Factor is 0.88)	(2) F32T8	0.49A	<20%	<b>0.10A</b>
ICN-2P32-SC	<i>Centium</i> Electronic	100% (Ballast Factor is 0.88)	(2) F32T8	0.49A	<10%	<b>0.05A</b>
Izt-2S32-SC + Dimming Control	Mark 7® 0-10V Electronic	100% (Ballast Factor is 1.0)	(2) F32T8	0.57A	<10%	<b>0.05A</b>
Izt-2S32-SC + Dimming Control	Mark 7® 0-10V Electronic	5% (Ballast Factor is 0.05)	(2) F32T8	0.12A	<20%	<b>0.02A</b>
REZ-2S32-SC (Ballast Only)	Mark 10® <i>Powerline</i> Electronic	100% (Ballast Factor is 1.0)	(2) F32T8	0.58A	<10%	<b>0.06A</b>
REZ-2S32-SC + Dimming Control	Mark 10® <i>Powerline</i> Ballast + Dimmer	100% (Ballast Factor is 1.0)	(2) F32T8	0.58A	<15%	<b>0.09A</b>
REZ-2S32-SC + Dimming Control	Mark 10® <i>Powerline</i> Ballast + Dimmer	5% (Ballast Factor is 0.05)	(2) F32T8	0.19A	<95%	<b>0.13A</b>

<sup>1</sup> For a more technical study demonstrating that a Mark 10® *Powerline* electronic dimming system produces less transformer heating over its entire dimming range than does an energy saving magnetic system that it replaces, see the article *THD in Advance Mark 10® Powerline Electronic Dimming Systems* by O.C. Morse. Re: [www.advancetransformer.com](http://www.advancetransformer.com)

<sup>2</sup> The Total Harmonic Current (THC) of a ballast is calculated by the following equation:

$$\frac{\text{Ballast Input Current}}{\text{Square Root of } (1 + 1/\text{THD}^2)}$$

An approximation of THC may be obtained by simply multiplying the ballast input current by %THD.

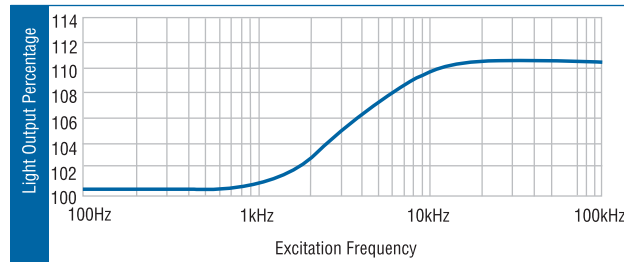
## Ballast Life

Advance fluorescent electronic and magnetic ballasts are designed and manufactured to engineering standards correlating to an average life expectancy of 50,000 hours of operation at maximum rated case temperature. Since Advance ballasts operate below their maximum case temperature in the majority of applications, increased ballast life can be expected. As a rule of thumb, ballast life is doubled for every 10°C reduction in ballast case operating temperature. However, there are many variables, such as input voltage, ambient temperature, etc. which affect ballast operating temperatures, and therefore ballast life.

## Lamp Operating Frequency

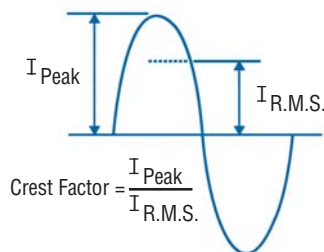
Electromagnetic ballasts and the lamps connected to them operate at an input voltage frequency of 60 Hertz (Hz), 60 cycles per second—which is the standard alternating voltage/current frequency provided in North America. Electronic ballasts, on the other hand, convert this 60 Hz input to operate lamps at much higher frequencies above 20 Kilohertz (kHz), 20,000 cycles per second. Advance designs operate above 20 kHz, but avoid certain ranges such as 30-40 kHz (infrared) and 54-62 kHz (theft deterrent systems) due to interference issues.

Because electronic ballasts function at high frequency, the fluorescent lighting systems that they operate can convert power to light more efficiently than systems operated by electromagnetic ballasts (See Chart Below). For example, lamps operated on electronic ballasts can produce over 10 percent more light than if operated on electromagnetic ballasts at the same power levels. In effect, today's electronic ballasts provide additional energy savings by matching the light output from electromagnetic ballasts while operating the lamps at lower power. This is the main reason why electronic ballast systems are more efficient than magnetic ballast system.



## Crest Factor

Lamp manufacturers use crest factor to determine ballast performance as it relates to lamp life. Lamp Current Crest Factor is a measurement of current supplied by a ballast to start and operate the lamp. It is basically the ratio of peak current to RMS (average) current. High crest factor currents may cause the lamp electrodes to wear out faster, reducing lamp life. Crest factor requirements are regulated by ANSI (American National Standards Institute) standards and specified by lamp manufacturers. For rapid start and instant start T8 lamps the ratio is 1.7 maximum, and for instant start slimline lamps, it is 1.85 maximum.



## Weight and Size Advantages

Since electronic components in electronic ballasts are smaller and lighter than the core-and-coil assembly in electromagnetic ballasts, electronic ballasts can weigh less than half as much as comparable electromagnetic models. Almost all Advance electronic ballasts have a smaller cross-section than electromagnetic ballasts but maintain the same mounting dimensions. This means that they can fit into all new fixture designs and can be easily retrofitted into existing fluorescent lighting systems.

## Controllability

The ability of a building's occupants to control how they light their space is becoming an increasingly important factor for organizations in determining what real estate they will lease, buy or invest in. The ability to dim the lights or easily shut them off completely is a trend fueled not just by a desire to help the environment, but also by significant economic benefits. These benefits include greater energy efficiency – in terms of reduced HVAC costs as well as energy savings for lighting – more comfortable and productive working environments, and compliance with ever tighter energy efficiency regulations. Advance offers three families of electronic controllable ballasts – ROVR™, Mark 7™ 0-10V and Mark 10™ Powerline – that can provide up to 65% energy savings over standard T8 fixed light output systems.

## Compatibility With Powerline Carrier Systems

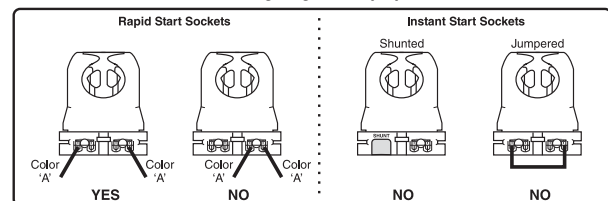
A powerline carrier system (PLC) uses electronic wiring devices to send information via a high frequency signal over the 120V or 277V electrical power distribution system of a building. For example, PLC systems are used in automatic clock systems (master time systems) to synchronize all of the clocks in a building or reset the time after a power outage. They eliminate the need for maintenance personnel to reset hundreds of clocks throughout a facility.

In a PLC system, a generator is used to impose a 1 to 4V high frequency signal on top of the existing voltage sine wave (60 Hz). This signal is generally in the 2500 to 9500Hz range, with some older systems operating at 19,500Hz or higher. Some electronic ballasts which are capacitive can absorb the signal from a PLC system. As a result, the signal becomes too weak to be "heard" by the receiver (like a timeclock) connected to the powerline.

## Instant Start vs. Rapid Start Sockets for Dimming

When using dimming ballasts in fixtures, sockets must be of the **RAPID START** type. Many fixtures with T-8 Instant Start electronic ballasts use jumpered or "shunted" Instant Start sockets. Controllable ballasts require two distinctly separate wires for each lamp socket. If you encounter shunted or jumpered sockets in a retrofit application, they must be removed and replaced with Rapid Start sockets.

**Improper socket application will damage the ballast and void the ballast warranty. Refer to ballast wiring diagram for proper installation.**



## Fluorescent Lamp Burn-In

Today, most lamp manufacturers do not require the burn-in of linear fluorescent lamps prior to dimming in order to attain rated lamp life and stable electrical measurements. However, some manufacturers compact fluorescent lamp sources do require a 100 hour burn-in prior to dimming. Consult your lamp manufacturer for their latest requirements.

## ORDERING INFORMATION

### How to Order

Advance has developed the industry's broadest distribution system for electronic ballasts. More than 3000 stocking distributors nationwide. For information on the distributor best able to serve your needs, please call 800-372-3331 or go to [www.advancetransformer.com/distributorsearch](http://www.advancetransformer.com/distributorsearch).

### Electronic Ballast Part Number Breakdown

**I** **CF** - **2** **S** **26** - **H1** - **LD**

#### CFL Mounting/Connector Options

BL = Bottom leads  
 BLS = Bottom leads with mounting studs  
 BS = Bottom mounting studs with single entry color coded connectors  
 EL = End leads  
 LD = Length mounting feet with SmartMate® dual entry color coded connectors  
 LS = Length mounting feet with single entry color coded connectors  
 QS = QuikStart

#### Linear Fluorescent Mounting/Connector Options

TP\* = Thermal Protected  
 2LS = 2 Level Switching

#### CFL Can Description

H1 = Hybrid metal / plastic case, size 1  
 L2 = Linear  
 M1 = Metal case, size 1  
 M2 = Metal case, size 2  
 M3 = Metal case, size 3  
 M4 = Metal case, size 4  
 M5 = Metal case, size 5  
 M6 = Metal case, size 6  
 S1 = Square, style 1  
 S2 = Square, style 2

#### Linear Fluorescent Can Description

90C = 90°C maximum case temperature rating  
 A = "A" can  
 D = "D" can  
 G = "G" can  
 HL = High light output  
 L = "L" can  
 LW = Low watt  
 MC = Micro can  
 RH\* = Reduced harmonics  
 S = Slimline  
 SC = Small can

#### Lamp Watts (Primary lamp)

#### Wiring Configuration

D = 2D, series  
 M = Modified parallel\*\*  
 P = Parallel  
 Q = Quad CFL, series  
 S = Series  
 T = Triple CFL, series  
 TTS = Long twin tube, series  
 TTP = Long twin tube, parallel

#### Maximum Number of Lamps

#### Family Name

CF = Compact Fluorescent	CN = Centium
DA = ROVR	DL = ROVR
EB = AmbiStar	ELB = AmbiStar
EL = Standard	EZ = Mark 10® Powerline
IC = Mark 5®	MB = AmbiStar
OP = Optanium	ZT = Mark 7® 0-10V

#### Input Voltage

G = 347V  
 H = IntelliVolt 347V to 480V 50/60 Hz  
 I = IntelliVolt 120V to 277V 50/60 Hz  
 J = IntelliVolt 277V to 480V 50/60 Hz  
 R = 120V  
 V = 277V

Corporate Offices  
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 +1 (847) 390-5000 (International)

- Plan your lighting installation carefully; consider using the services of a qualified lighting designer
- Consult your local electric utility regarding demand side management rebate programs.
- Select the Advance electronic ballast which best matches the requirements of your application. The technical specifications in this catalog (located on pages 8-4 to 8-22) will be useful in obtaining bids from electrical contractors.
- Contact your local Advance distributor. You will find them to be a helpful supplier of both products and information.

\* Many current and all future electronic ballast part numbers will not use the "RH-TP" suffixes even though these ballasts will be thermally protected.

\*\* Parallel Wiring Configuration. However, if one lamp fails, all other lamps in the circuit will extinguish.

# T8/ES



## HIGH FREQUENCY ELECTRONIC BALLASTS

# For 25W - 48" Lamps

HIGH POWER FACTOR SOUND RATED A



ELECTRONIC FLUORESCENT

No. of Lamps	Input Volts	Lamp Starting Method	Ballast Family	Catalog Number	Input Power ANSI (Watts)	Ballast Factor	Max. THD %	Line Current (Amps)	Min. Starting Temp. (°F/°C)	Dim.	Wiring Dia.
<b>F32T8/ES (25W - 48")</b>											
1	120-277	IS	Optanium	IOP-1P32-LW-SC	21	0.77	10	0.17-0.07	60/16	B	63
				IOP-1P32-SC	23	0.87	10	0.20-0.09			
				IOP-1P32-HL-SC	32	1.21	10	0.26-0.12			
				IOP-2P32-LW-SC	24	0.90	10	0.20-0.09			*64
				IOP-2P32-SC	27	1.05	10	0.23-0.10			
		PS		IOP-2P32-HL-SC	37	1.40	15	0.31-0.14			20
				IOP-1S32-LW-SC	21	0.72	10	0.17-0.07			
				IOP-1S32-SC	24	0.88	10	0.20-0.08			39
				IOP-2S32-LW-SC	21	0.73	10	0.17-0.08			
2	120-277	IS	Optanium	IOP-2P32-LW-SC	38	0.77	10	0.32-0.14	60/16	B	64
				IOP-2P32-SC	44-43	0.87	10	0.37-0.06			
				IOP-2P32-HL-SC	60	1.19	10	0.50-0.22			
				IOP-3P32-LW-SC	43	0.86	10	0.36-0.16			*65
				IOP-3P32-SC	49	1.00	10	0.42-0.18			
		PS		IOP-3P32-HL-90C-SC	70	1.32	10-20	0.59-0.27			21
				IOP-2S32-LW-SC	39-38	0.71	10	0.32-0.14			
				IOP-2S32-SC	45-44	0.88	10	0.38-0.16			65
				3	120-277	IS	Optanium	IOP-3P32-LW-SC			
IOP-3P32-SC	65-64	0.87	10					0.55-0.24			
IOP-3P32-HL-90C-SC	95-93	1.20	10					0.79-0.35			
IOP-4P32-LW-SC	62-61	0.85	10					0.52-0.22	*66		
IOP-4P32-SC	70-69	0.97	10					0.59-0.26			
PS	IOP-4P32-HL-90C-G	101-100	1.27			10		0.85-0.37	G		
	IOP-3S32-LW-SC	57-56	0.71			10		0.48-0.21		B	
	IOP-3S32-SC	67-66	0.89			10		0.56-0.25	30		
	4	120-277	IS			Optanium		IOP-4P32-LW-SC		77-75	0.77
IOP-4P32-SC				87-85	0.87		10	0.73-0.31			
PS			IOP-4P32-HL-90C-G	124-122	1.19		10	1.05-0.45	G		
			IOP-4S32-LW-SC	74-73	0.71		10	0.62-0.27		B	
			IOP-4S32-SC	87-85	0.87		10	0.73-0.31			

Note: The use of Optanium (IOP) models is recommended to reduce striation in energy-saving T8 lamps (25W, 28W, or 30W). Remote or tandem wiring of energy-saving T8 lamps (25W, 28W or 30W) is only recommended for Optanium (IOP) models.

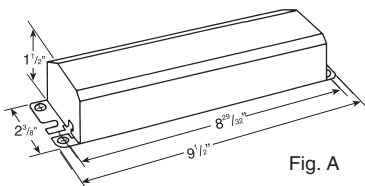


Fig. A

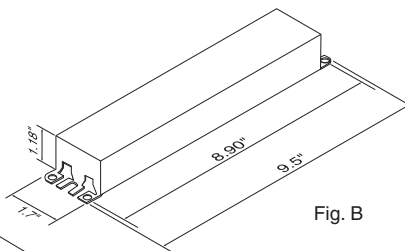


Fig. B

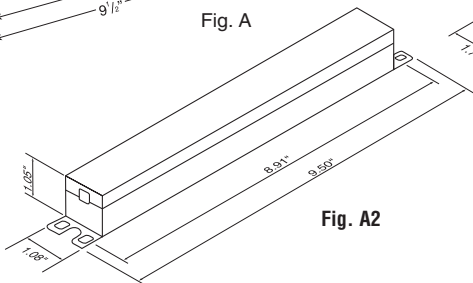


Fig. A2

See page 1-57 for Wiring Diagrams

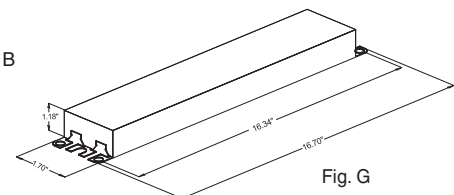


Fig. G

Refer to pages 8-24 to 8-30 for lead lengths and shipping data

# For 28W - 48" Lamps

# T8/ES



HIGH POWER FACTOR SOUND RATED A



ELECTRONIC  
FLUORESCENT

No. of Lamps	Input Volts	Lamp Starting Method	Ballast Family	Catalog Number	Input Power ANSI (Watts)	Ballast Factor	Max. THD %	Line Current (Amps)	Min. Starting Temp. (°F/°C)	Dim.	Wiring Dia.
<b>F32T8/ES (28W - 48")</b>											
1	120-277	IS	Optanium	IOP-1P32-LW-SC	22	0.77	10	0.19-0.08	60/16	B	63
				IOP-1P32-SC	25	0.87	10	0.22-0.10			
				IOP-1P32-HL-SC	33	1.21	10	0.28-0.12			
				IOP-2P32-LW-SC	26	0.90	10	0.22-0.10			*64
				IOP-2P32-SC	31	1.05	10	0.26-0.11			
				IOP-2P32-HL-SC	39	1.38	10	0.33-0.15			
		PS		IOP-1S32-LW-SC	21	0.72	10	0.18-0.07			20
				IOP-1S32-SC	25	0.88	10	0.20-0.09			39
				IOP-2S32-LW-SC	22	0.73	10	0.18-0.08			
2	120-277	IS	Optanium	IOP-2P32-LW-SC	42	0.77	10	0.35-0.15	60/16	B	64
				IOP-2P32-SC	48-47	0.87	10	0.41-0.18			
				IOP-2P32-HL-SC	65-64	1.19	10	0.55-0.24			
				IOP-3P32-LW-SC	47	0.86	10	0.40-0.18			*65
				IOP-3P32-SC	55-54	1.00	10	0.46-0.20			
				IOP-3P32-HL-90C-SC	74-73	1.31	10-15	0.62-0.27			
		PS		IOP-2S32-LW-SC	41-40	0.71	10	0.34-0.15			21
				IOP-2S32-SC	49-48	0.88	10	0.41-0.18			
				3	120-277	IS	Optanium	IOP-3P32-LW-SC			64-63
IOP-3P32-SC	72-71	0.87	10					0.61-0.26			
IOP-3P32-HL-90C-SC	99-97	1.20	10					0.83-0.36			
IOP-4P32-LW-SC	69-68	0.85	10					0.58-0.25	*66		
IOP-4P32-SC	79-78	0.97	10					0.66-0.28			
IOP-4P32-HL-90C-G	107-106	1.24	10					0.90-0.39			
PS	IOP-3S32-LW-SC	62-61	0.71			10		0.51-0.22	30		
	IOP-3S32-SC	72-71	0.89			10		0.60-0.26			
	4	120-277	IS			Optanium		IOP-4P32-LW-SC	84-82	0.77	10
IOP-4P32-SC				96-94	0.87		10	0.81-0.35			
IOP-4P32-HL-90C-G				130-129	1.19		10	1.10-0.47			
PS			IOP-4S32-LW-SC	80-79	0.71		10	0.67-0.29	138		
			IOP-4S32-SC	97-96	0.88		10	0.82-0.35			

Note: The use of Optanium (IOP) models is recommended to reduce striation in energy-saving T8 lamps (25W, 28W, or 30W). Remote or tandem wiring of energy-saving T8 lamps (25W, 28W or 30W) is only recommended for Optanium (IOP) models.

See page 1-52 for Dimensions  
See page 1-57 for Wiring Diagrams

Refer to pages 8-24 to 8-30 for lead lengths and shipping data





# T8/ES



## HIGH FREQUENCY ELECTRONIC BALLASTS

# For 30W - 48" Lamps

HIGH POWER FACTOR SOUND RATED A



ELECTRONIC  
FLUORESCENT

No. of Lamps	Input Volts	Lamp Starting Method	Ballast Family	Catalog Number	Input Power ANSI (Watts)	Ballast Factor	Max. THD %	Line Current (Amps)	Min. Starting Temp. (°F/°C)	Dim.	Wiring Dia.				
<b>F32T8/ES (30W - 48")</b>															
1	120	IS	Standard	REL-1P32-SC	29	0.92	20	0.25	60/16	B	63				
				REL-1P32-HL-SC	39	1.20	20	0.33			*64				
				REL-2P32-SC	35	1.10	25	0.31							
				REL-2P32-HL-SC	45	1.41	20	0.38							
		PS	Centium	RCN-1S32-SC	32	0.90	10	0.27			20				
				VEL-1P32-SC	29	0.92	20	0.11			60/16	B	63		
	IS	Standard	VEL-1P32-HL-SC	39	1.20	20	0.14	*64							
			VEL-2P32-SC	35	1.10	25	0.13								
			VEL-2P32-HL-SC	45	1.41	20	0.17								
	PS	Centium	VCN-1S32-SC	32	0.90	10	0.12	20							
	120-277		IS	Centium	ICN-132-MC	27	0.88	10	0.23-0.10	60/16	B	A2	63		
					ICN-1P32-LW-SC	25	0.77	10	0.21-0.09				*64		
					ICN-1P32-SC	29	0.90	10	0.24-0.11						
					ICN-2P32-LW-SC	29-28	0.85	15-20	0.24-0.11						
					ICN-2P32-SC	33	1.03	10	0.28-0.12						
					IOP-1P32-LW-SC	24	0.77	10	0.20-0.09			63			
				IOP-1P32-SC	27	0.87	10	0.23-0.10							
				IOP-1P32-HL-SC	37-36	1.20	10	0.31-0.13	*64						
				IOP-2P32-LW-SC	28	0.90	10	0.24-0.10							
				IOP-2P32-SC	33	1.05	10	0.28-0.12							
				IOP-2P32-HL-SC	42	1.38	10	0.35-0.16							
				PS	Optanium	IOP-1S32-LW-SC	23	0.72	10			0.19-0.08	20		
						IOP-1S32-SC	27	0.88	10			0.22-0.10			
						IOP-2S32-LW-SC	24-23	0.73	10			0.20-0.09		39	
						IOP-2S32-SC	27	0.90	10			0.23-0.10		20	
						Mark 5	IIC-132-SC	30	0.88			10		0.26-0.11	20
								GEL-1P32-SC	32			0.87		20	0.10
				IS	Standard	GEL-2P32-SC	36	1.10	20			0.10	*64		
	GCN-1P32-SC	32	0.87			10	0.10	63							
	Centium	GCN-2P32-SC	37	0.91	10	0.11	*64								
GCN-1S32			32	0.90	10	0.09	A	20							
RS															

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See page 1-52 for Dimensions  
See page 1-57 for Wiring Diagrams

Refer to pages 8-24 to 8-30 for lead lengths and shipping data

# For 30W - 48" Lamps

# T8/ES



HIGH POWER FACTOR SOUND RATED A



ELECTRONIC  
FLUORESCENT

No. of Lamps	Input Volts	Lamp Starting Method	Ballast Family	Catalog Number	Input Power ANSI (Watts)	Ballast Factor	Max. THD %	Line Current (Amps)	Min. Starting Temp. (°F/°C)	Dim.	Wiring Dia.	
<b>F32T8/ES (30W - 48")</b>												
2	120	IS	Standard	REL-2P32-SC	54	0.87	20	0.46	60/16	B	64	
				REL-2P32-HL-SC	72	1.20	20	0.60			*65	
				REL-3P32-SC	61	1.03	20	0.51				
				REL-3P32-HL-SC	80	1.32	20	0.67				
		PS	Centium	RCN-2S32-SC	60	0.88	10	0.51			21	
	277	IS	Standard	VEL-2P32-SC	54	0.87	20	0.20	60/16	B	64	
				VEL-2P32-HL-SC	72	1.20	20	0.26			*65	
				VEL-3P32-SC	61	1.03	20	0.22				
				VEL-3P32-HL-SC	80	1.32	20	0.29				
		PS	Centium	VCN-2S32-SC	60	0.88	10	0.22			21	
	120-277	IS	Centium	ICN-2M32-MC	54	0.88	10	0.45-0.20	60/16	B	A2	64
				ICN-2P32-LW-SC	47-46	0.77	10	0.39-0.17			*65	
				ICN-2P32-SC	54	0.88	10	0.45-0.20				
				ICN-3P32-LW-SC	52	0.83	10	0.44-0.19				
				ICN-3P32-SC	61	1.01	10	0.51-0.22				
			Optanium	IOP-2P32-LW-SC	45	0.77	10	0.38-0.17			*65	
				IOP-2P32-SC	52-51	0.87	10	0.44-0.19				
				IOP-2P32-HL-SC	72-70	1.19	10	0.60-0.26				
				IOP-3P32-LW-SC	51	0.85	10	0.43-0.19			64	
				IOP-3P32-SC	59-58	1.00	10	0.50-0.21				
		PS	Mark 5	IOP-3P32-HL-90C-SC	78-77	1.31	10	0.65-0.29				
				IOP-2S32-LW-SC	44-43	0.71	10	0.36-0.16			*65	
				IOP-2S32-SC	52	0.88	10	0.44-0.19				
	347	IS	Standard	GEL-2P32-LW-RH-TP	49	0.76	20	0.14	60/16	A	64	
				GEL-2P32-SC	56	0.88	20	0.17			*65	
				GEL-3P32-SC	62	0.98	20	0.20				
				GEL-2S32-RH-TP	62	0.89	20	0.18			21	
		Centium	GCN-2P32	59	0.87	10	0.18	64				
GCN-3P32			62	0.98	10	0.20	*65					
RS			GCN-2S32	60	0.90	10	0.17	21				

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